

## Body Surface Potential Mapping Data Conversion Method

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***Abstract.** In body surface potential mapping, data conversion can be required whenever merging data sets taken by slightly different data acquisition systems. In this case, we face with a kind of conversion problem. This paper describes a method for solving the problem according to the least-square principle, so the datasets of physically different body surface potential mapping systems become compatible, thus their records can be handled the same way.*

*Keywords:* ECG, Body surface potential mapping systems, different electrode distribution, Data conversion

### 1. Introduction

High spatial and temporal resolution body surface potential mapping play an important role in sudden cardiac death risk assessment. These elaboration of decision rules require a high number of validated measurements. To achieve the statistically significant number of records, pooling of data bases recorded in different groups is a realistic approach. However, if the electrode layouts are not strictly identical in the cooperating groups, a measurement data conversion is needed for making the two systems compatible. In the following section, a method will be described for solving this problem with the help of our example, done at the Department of Electrical Engineering and Information Systems, University of Pannonia.

### 2. Subject and Methods

In the framework of our scientific cooperation with the Polish research group led by Professor Roman Maniewski we had to make compatible the records taken in Hungary and Poland. Since the Polish research group uses a slightly different lead arrangement, we had to elaborate the conversion method.

#### *The two lead arrangements*

The lead arrangements of our and the Polish body surface potential acquisition system is shown in Fig. 1 and Fig. 2.

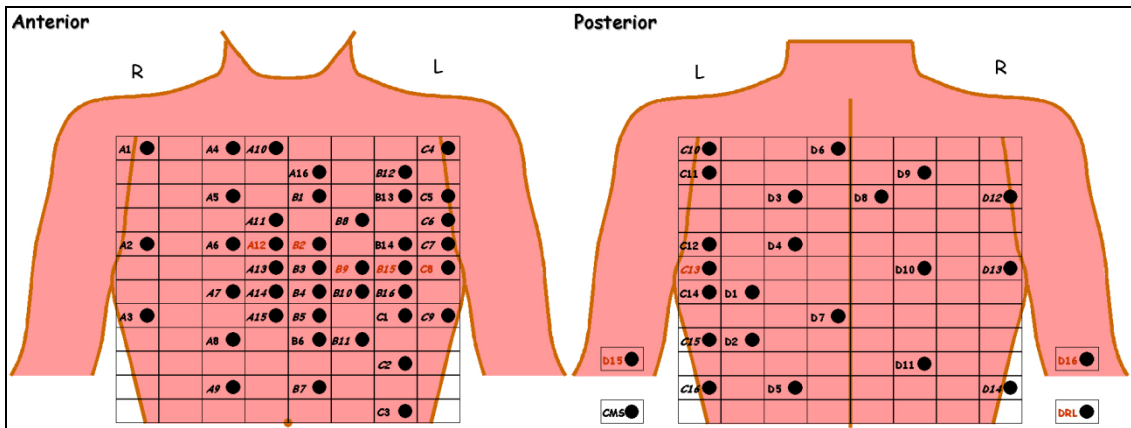


Fig. 1. Electrode positions of our Biosemi Mark-8 body surface potential mapper. Electrodes A1-D14 are on the torso, D15 is on the left arm and D16 is on the right arm. The leads are unipolar (reference is the WCT) [1].

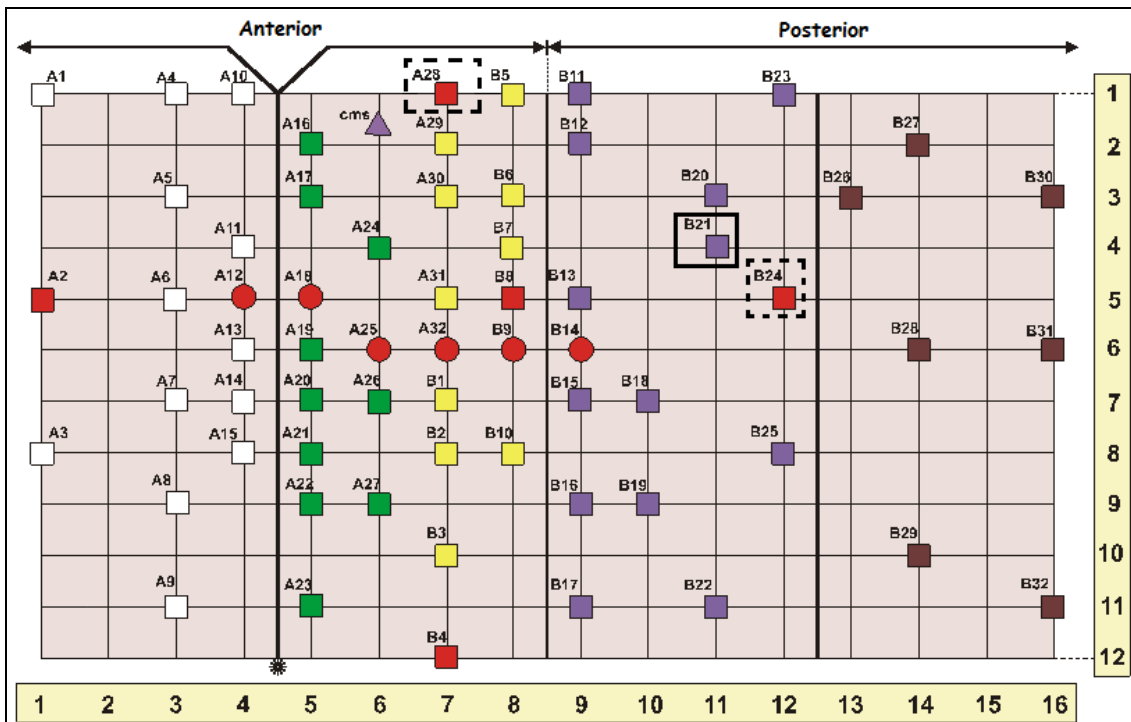


Fig. 2. Electrode positions of the Polish body surface potential mapper and the difference between the electrode locations of the two systems. Dashed frames mark the two leads missing from our system and solid frame signs the channel which is one unit higher than the corresponding D4 channel in our system. The other 61 leads are in the same positions regarding the two systems [2].

*Principle of the method*

There is a method based on least squares for estimating unknown lead data from known ones. The method was published by Robert L. Lux, et al. [3]. Its principle is as follows:

$$\phi_{est} = T \cdot \phi_m \tag{1}$$

where

$\varphi_{est}$  :  $k \times n$  matrix of estimated leads  
 $\varphi_m$  :  $m \times n$  matrix of measured leads  
 $T$  :  $k \times m$  estimating matrix  
 $k$  : number of estimated leads  
 $m$  : number of measured leads  
 $n$  : number of sampling points

To determine  $T$  we need a covariance matrix  $K$ , regarding all channels (both measured and estimated).  $T$  is defined as follows:

$$T = K'_{est} \cdot K_m^{-1} \quad (2)$$

where

$K_{est}$  :  $m \times k$  segment of  $K$  regarding estimated leads  
 $K_m$  :  $m \times m$  segment of  $K$  regarding measured leads

We searched for a method for estimating our D4 lead from the 61 common leads (see Fig. 2), so we would be able to get the same 62 leads from the Polish records that we have. The steps of finding this method can be seen below in detail.

### Determinating $K$

The more measurements we use, the more accurate our estimate will be, so we concatenated 52 records of our measurements considering leads A1-D14. This way we got a  $62 \times 10982400$  matrix. Then we interpolated this data to 192 lead, so the matrix became  $192 \times 10982400$ . After that we calculated the covariance matrix  $K$  ( $192 \times 192$ ):

$$K = \begin{bmatrix} \begin{bmatrix} k_{1,1} & k_{1,2} & \cdots & k_{1,62} \\ k_{2,1} & k_{2,2} & \cdots & k_{2,62} \\ \vdots & \vdots & \ddots & \vdots \\ k_{62,1} & k_{62,2} & \cdots & k_{62,62} \end{bmatrix} & \begin{bmatrix} k_{1,63} & k_{1,64} & \cdots & k_{1,192} \\ k_{2,63} & k_{2,64} & \cdots & k_{2,192} \\ \vdots & \vdots & \ddots & \vdots \\ k_{62,63} & k_{62,64} & \cdots & k_{62,192} \end{bmatrix} \\ \begin{bmatrix} k_{63,1} & k_{63,2} & \cdots & k_{63,62} \\ k_{64,1} & k_{64,2} & \cdots & k_{64,62} \\ \vdots & \vdots & \ddots & \vdots \\ k_{192,1} & k_{192,2} & \cdots & k_{192,62} \end{bmatrix} & \begin{bmatrix} k_{63,63} & k_{63,64} & \cdots & k_{63,192} \\ k_{64,63} & k_{64,64} & \cdots & k_{64,192} \\ \vdots & \vdots & \ddots & \vdots \\ k_{192,63} & k_{192,64} & \cdots & k_{192,192} \end{bmatrix} \end{bmatrix} = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \quad (3)$$

The data is sorted like leads 1-62 are the leads before interpolation and leads 63-192 are the additional ones. Considering Fig. 1 it means, that lead 1 is A1, lead 2 is A2, ... and lead 62 is D14. And for the additional ones: lead 63 is the empty cell just below A1, lead 64 is two cells below A1, ... and finally lead 192 is just below D14.

Note that interpolation was unnecessary for this progress (only  $K_{11}$  will be used below), but we did it for further applicability.

### Determinating $K_m$ and $K_{est}$

$K_m$  is quadratic and it represents the measured data, so we have to choose it so that it shall contain the covariances of the leads that will be measured (known) in the future. In this case

the measured leads will be the 61 common leads, thus  $K_m$  will be  $61 \times 61$ . Considering Fig. 2 and Eq. 3 it can be seen that the matrix we are looking for is almost the same as  $K_{II}$  ( $62 \times 62$ ). The only difference is, that  $K_{II}$  contains the data of D4 too. It poses a problem, because that is the lead we would like to estimate. Since the covariances of D4 are in the 52th row and column, we can simply remove them, and the result will be  $K_m$ .

As written above,  $K_{est}$  is an  $m \times k$  matrix containing the covariances regarding estimated leads, where  $m$  is the number of measured leads and  $k$  is the number of estimated leads. Because we would like to estimate one lead,  $K_{est}$  will be  $61 \times 1$ . Due to the estimated lead will be D4, we can simply determine this matrix at the previously written  $K_m$  calculation: we have to remove the 52nd row from  $K_{II}$  first, then save the 52nd column as  $K_{est}$ , and remove the 52nd column from  $K_{II}$  after that.

Finally, substituting  $K_{est}$  and  $K_m$  to Eq. 2,  $T$  can be calculated.

### 3. Results

The covariance matrix was calculated from 52 measurements which means a relatively high population, therefore the estimation with the  $T$  matrix is accurate enough. Namely, the correlation between the estimated and measured data is 0.98.

### 4. Discussion

Whenever conversion has to be made between our and another "foreign" body surface potential mapping systems, a  $T$  matrix should be calculated as described above. During the calculation of the matrix, the "measured" data should represent the common channels of the two systems, while the "estimated" data mean the ones that exist in our system, but do not exist in the Polish one. The ones that appear only in the Polish system, can be simply neglected. After determination, the same  $T$  matrix can be used for any measurement of that particular device.

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